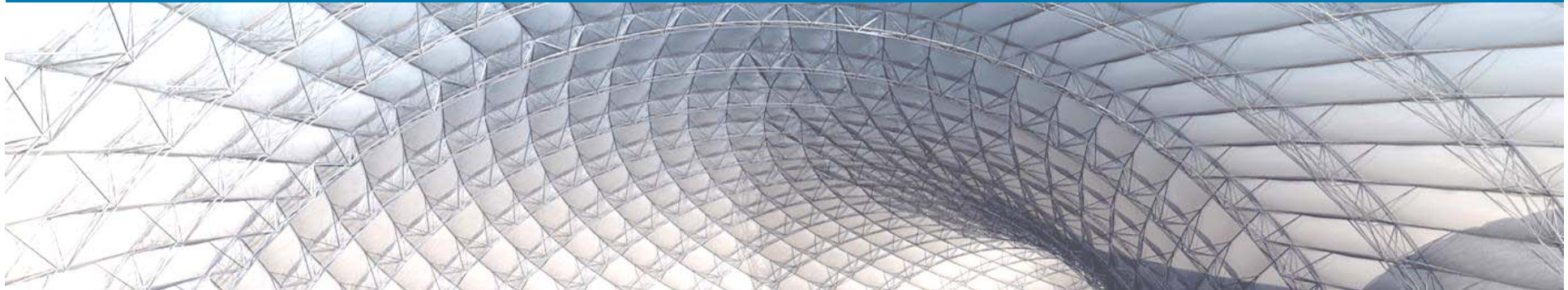


Innovative Use of Aerogel in Passive and Active Solar Storage Walls

Mark Dowson - CIBSE Building Simulation Group – 2nd June 2011



Buro Happold





Presentation outline:

- My background
- Research focus
- Two modelling case studies
 - Passive solar storage wall (i.e. a Trombe wall)
 - Active solar-air collector
- Questions



My background:

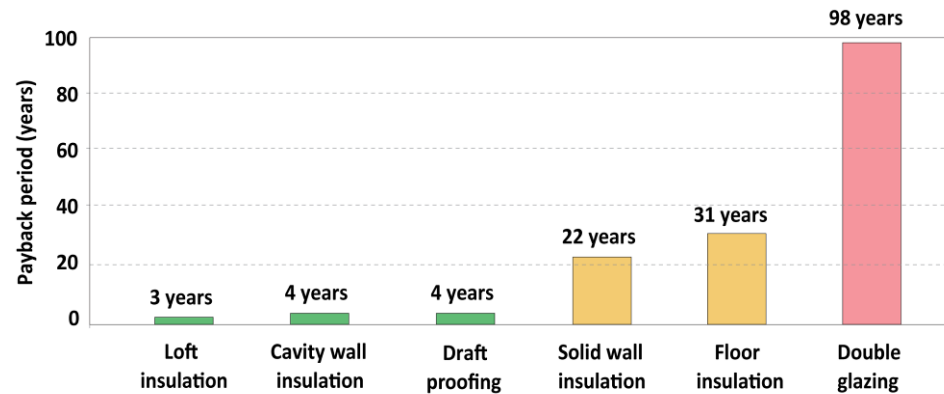
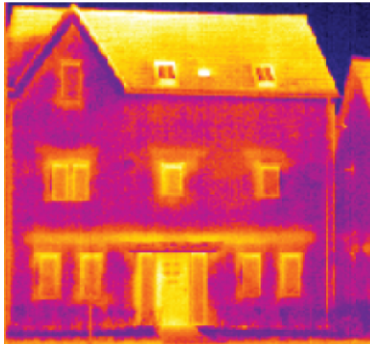
- Research engineer based in industry
- Currently undertaking an Engineering Doctorate (EngD) in Environmental Technology
- Industrial project sponsored by Brunel University and Buro Happold Ltd

Buro Happold:

- Global engineering consultancy for the built environment
- Sustainability and Building Physics team (London)

Focus of my research:

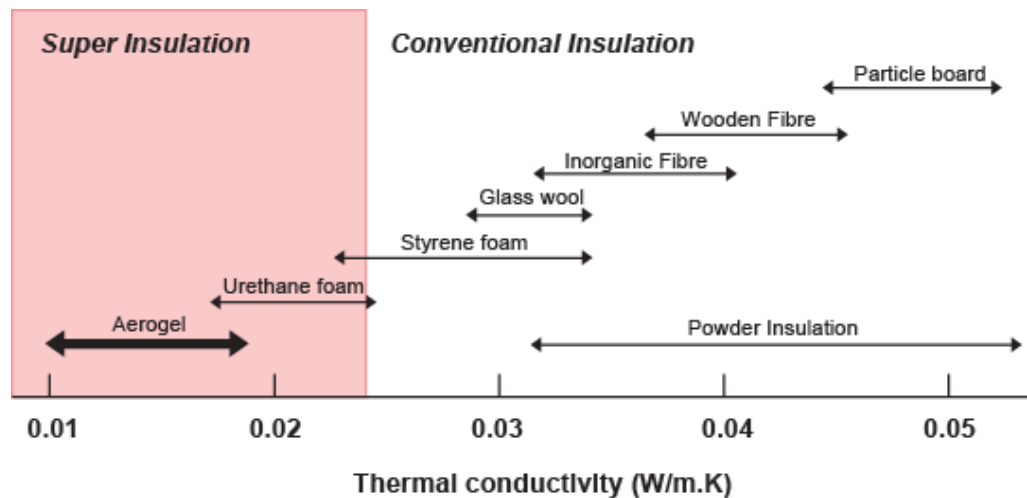
- Developing and testing new building fabric technologies incorporating high performance *silica aerogel insulation* to reduce demand for heating and artificial lighting in buildings



- Millions of homes in the UK are poorly insulated and expensive to heat
- Some conventional solutions to improve these homes are not cost effective

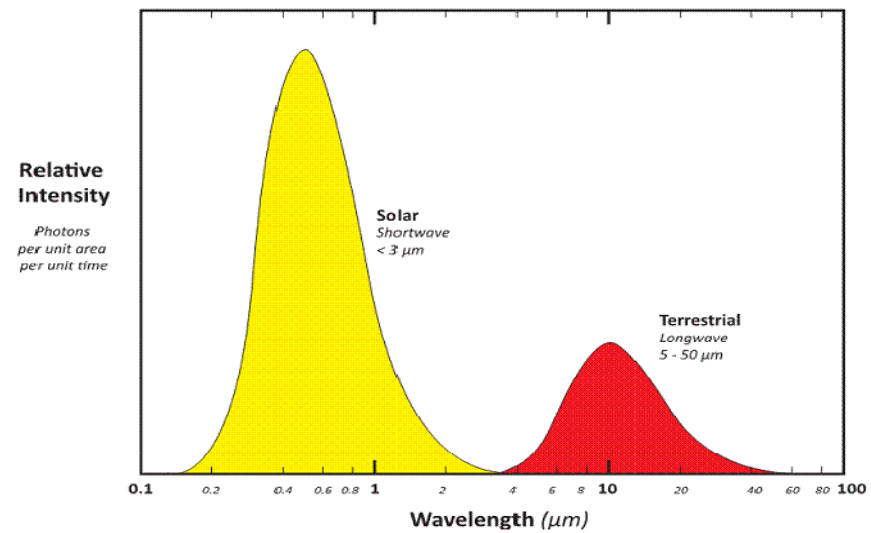
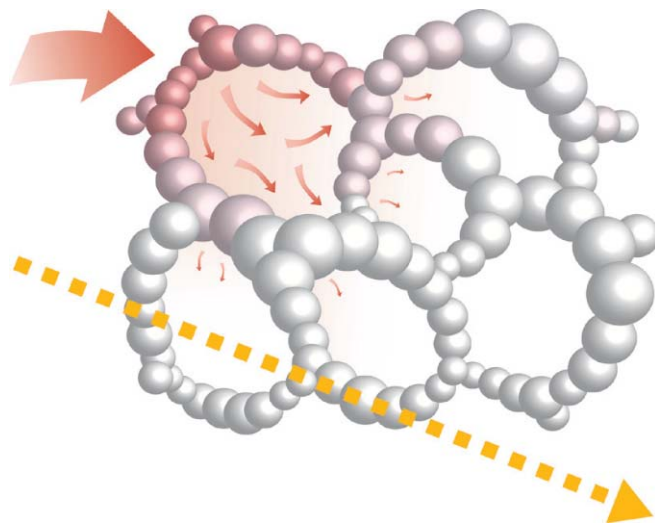
What is aerogel?

- Transparent “super-insulation” material
- Invented in the 1930s; only now emerging in the construction market
- Translucent granules are mass produced
- Solid tiles can be produced, but they are fragile and expensive, thus are not commercially available



How does it work?

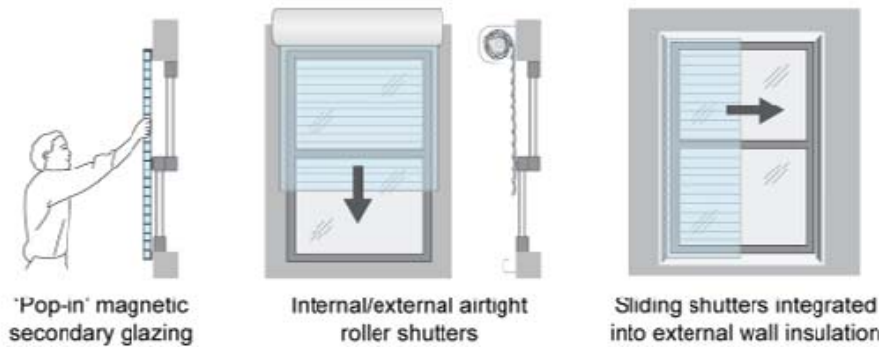
- Material contains a nanoporous structure – up to 99% air (1% silica)
- Nanosized pores block heat transfer by **convection**, **conduction** and **long-wave thermal radiation**
- Silica structure is highly transparent to **light** and **short-wave solar radiation**



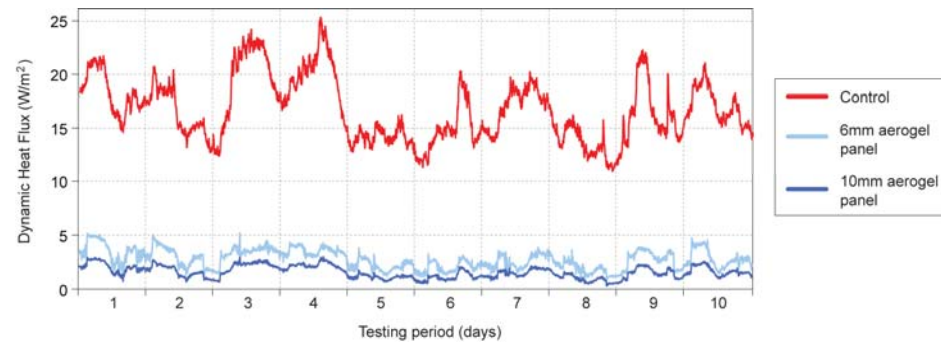
How can it be used?



Concepts to insulate existing windows:



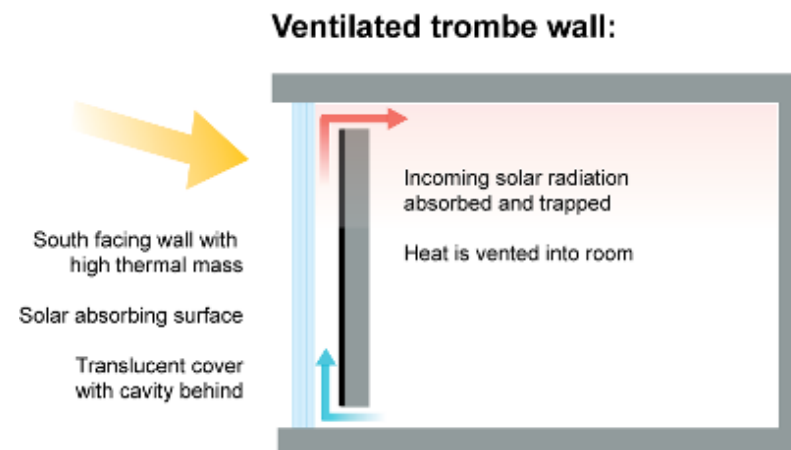
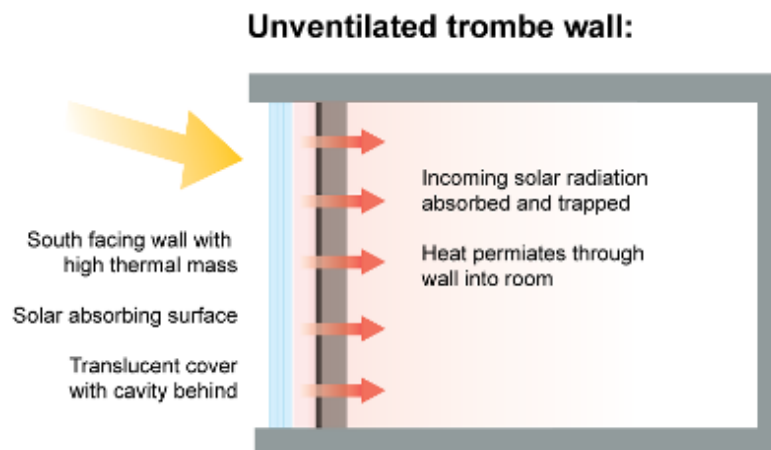
Measurements show an 80% reduction in heat loss!



Concepts for passive solar storage:

- High performance cover in south facing solar storage walls
- Aerogel has a lower solar transmission to standard single glazing but significantly reduces heat losses

*Let solar energy in.
Trap it.
Let it accumulate.
Use it*

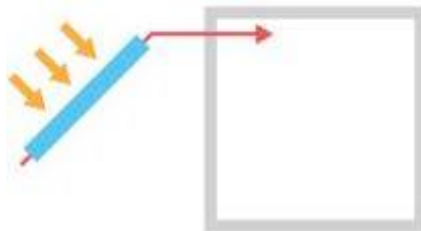


Concepts for active solar collection:

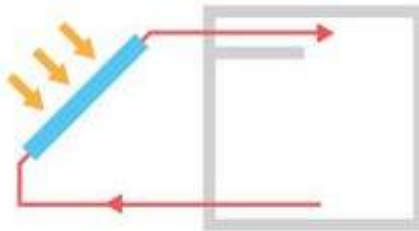
- Supply free solar heated warm air to a space instantaneously
- Storage can be introduced through PCM in collector or ductwork
- Air-water heat exchangers can avoid wasting heat in summer

*Let solar energy in.
Trap it.
Let it accumulate.
Use it*

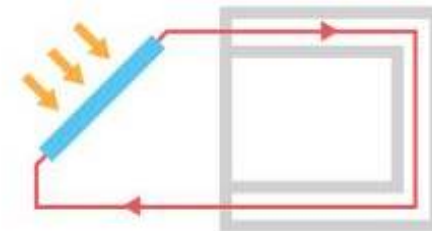
Solar heating of outside air supplied directly to space



Solar heating of room air returned via thermal storage in roof



Solar heated air circulated through cavity in the building envelope



CASE STUDY 1: Aerogel Trombe wall

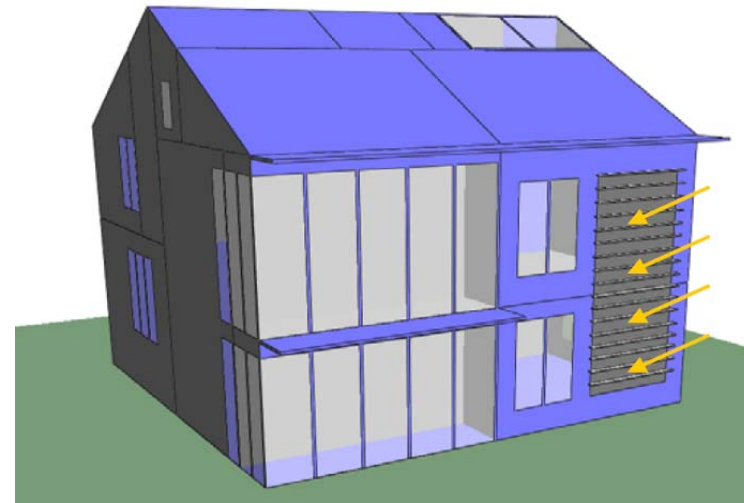
Riches Hawley Mikhail Architects

Robinson Associates Engineers

- Concept currently planned for a new eco-home in the UK
- Property will be highly insulated and have high thermal mass
- Aerogel Trombe wall is anticipated to reduce need for heating during cold-mild sunny days

Approach used:

- Parametric calculator built in Excel
- Model combines building parameters obtained through IES Virtual Environment software with average solar radiation and degree-day data for the site.
- Max allowable area = **7.5m²**

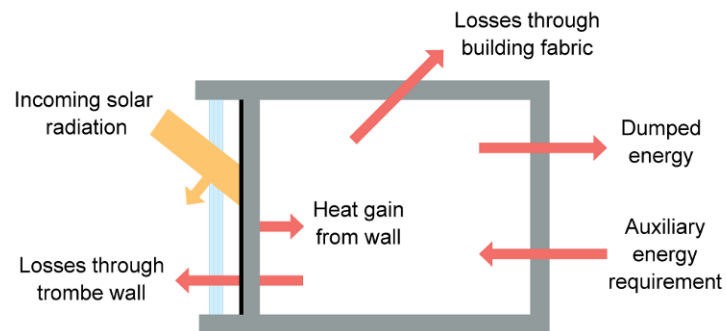


Overview of method:

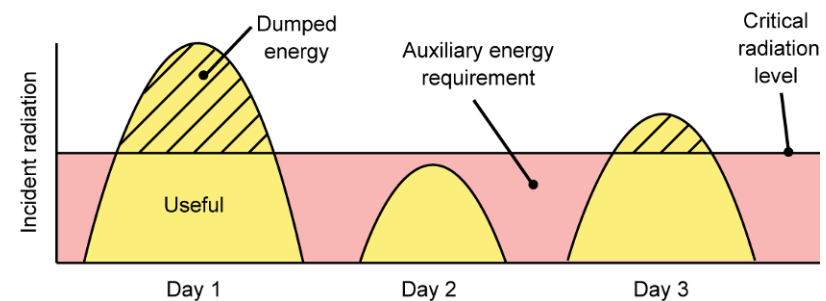
Chapter 22: Un-utilizability design method for collector-storage walls

- Method assumes system is unvented and heat transfer through the wall is linear
- Calculates a buildings monthly-average heat load with + without a Trombe wall, based upon:
 - Absolute upper and lower limits of the building and walls thermal capacity
 - Storage-dump ratio, defined by the systems actual thermal capacity

Trombe wall energy balance:



Storage-dump concept (for zero capacitance system):





Characterise site

- latitude
- longitude
- ground reflectance

Characterise building

- Heat loss parameter
- Thermal capacity
- Stat set points
- Allowable temp swing

Characterise wall

- Area
- Thickness
- Heat capacity
- Density
- Conductivity
- Loss co-efficient

Characterise cover transmission

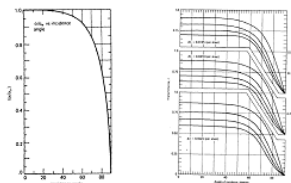
- Solar transmission
- Solar absorbance
- Solar reflectance
- Overall product in terms of beam, diffuse and ground reflected radiation

| Characterise Site | | | |
|-------------------|--|---|-------|
| | | | Input |
| 1 | Latitude angle | φ | 54.3 |
| 2 | Longitude angle (degrees east) | λ | 0.07 |
| 3 | Standard deviation for local time zone | D | 0.00 |
| 4 | Ground reflectance | G | 0.20 |

| Characterise Building | | | |
|-----------------------|--|--------------------|-------|
| | | | Input |
| 5 | Maximum allowable inside temperature | T _{i,max} | 18.3 |
| 6 | Minimum temperature rating | T _{i,min} | 16.0 |
| 7 | Building loss coefficient | U _{loss} | 0.34 |
| 8 | Effective heat capacity of building (thermal mass parameter) | C _b | 9500 |
| 9 | Loss coefficient (losses other than walls) | U _{other} | 0.1 |

| Characterise Trombe Wall | | | |
|--------------------------|--|----------------|-------|
| | | | Input |
| 10 | Bricklay | p _b | 2400 |
| 11 | Modulus of elasticity | E _b | 8.05 |
| 12 | Thickness | L _b | 0.45 |
| 13 | Conductivity | k _b | 0.75 |
| 14 | Surface absorptance | α _b | 0.85 |
| 15 | Heat capacity of brick (per unit volume) | C _b | 9500 |
| 16 | Thermal mass parameter | U _b | 0.22 |

| Transmittance-Absorbance Calculations | | | |
|---------------------------------------|--|------------------|---------------|
| | | | Output |
| 17 | Cover material | P | Polycarbonate |
| 18 | Angle of incidence | θ _i | 58.8 |
| 19 | Number of covers | N | 2 |
| 20 | Preparationally corrected transmittance coefficient (reference 4.16) | T ₀ | 0.88 |
| 21 | Cover thickness (reference table values used where appropriate) | L | 0.002 |
| 22 | Reference index (reference 4.16) | n | 1.5 |
| 23 | Angle of refraction | θ _r | 36.8 |
| 24 | Preparationally corrected transmittance coefficient | T ₁ | 0.88 |
| 25 | Preparationally corrected transmittance coefficient | T ₂ | 0.88 |
| 26 | Preparationally corrected transmittance coefficient | T ₃ | 0.88 |
| 27 | Reference index | n ₁ | 1.5 |
| 28 | Transmittance (preparationally corrected losses only) | T ₄ | 0.88 |
| 29 | Transmittance (preparationally corrected losses through glazing) | T ₅ | 0.88 |
| 30 | Absorbance | A | 0.12 |
| 31 | Transmittance | D | 0.88 |
| 32 | Reflectance | R | 0.12 |
| 33 | Angle of incidence for beam radiation | θ _{i,b} | 57.88 |
| 34 | Solar absorption coefficient (figure 4.15.1) | α ₀ | 0.83 |
| 35 | Transmittance factor (figure 4.15.1) | τ ₀ | 0.88 |
| 36 | Transmittance factor (figure 4.15.1) | τ ₁ | 0.83 |
| 37 | Transmittance factor (figure 4.15.1) | τ ₂ | 0.83 |
| 38 | Angle of incidence for diffuse radiation | θ _{i,d} | 57.88 |
| 39 | Solar absorption coefficient (figure 4.15.1) | α ₀ | 0.83 |
| 40 | Transmittance factor (figure 4.15.1) | τ ₀ | 0.83 |
| 41 | Transmittance factor (figure 4.15.1) | τ ₁ | 0.83 |
| 42 | Transmittance factor (figure 4.15.1) | τ ₂ | 0.83 |



Parametric calculator

Characterise months

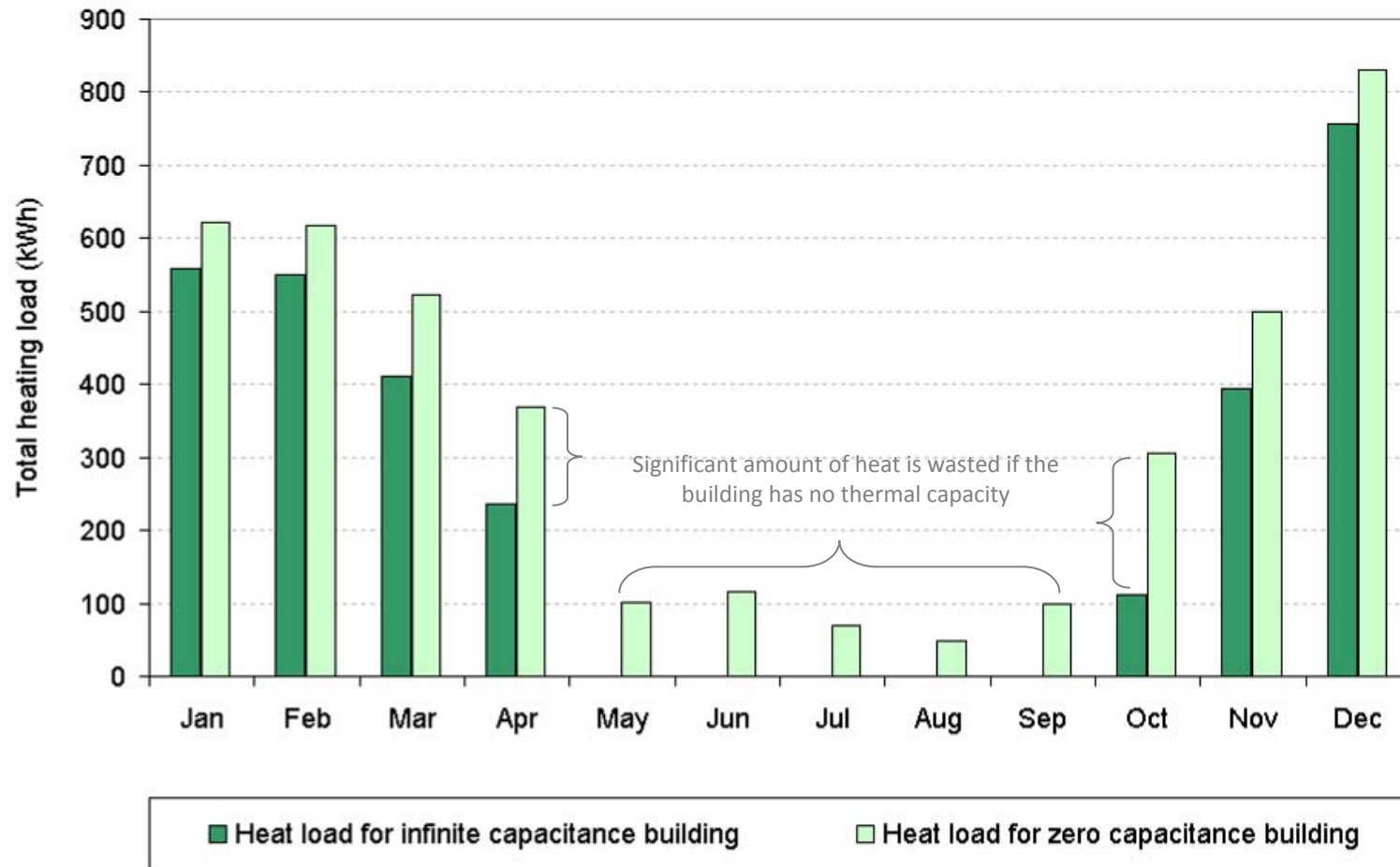
| | | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|----|---|----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 43 | Number of days in month | 31 | 28 | 31 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | 31 |
| 44 | Mid-month day in year | 57 | 87 | 117 | 147 | 177 | 207 | 237 | 267 | 297 | 327 | 357 | 387 |
| 45 | Days from Dec | 274 | 244 | 214 | 184 | 154 | 124 | 94 | 64 | 34 | 4 | 24 | 54 |
| 46 | Hourly temperature for degree days calculation | T _a | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 |
| 47 | Monthly temperature loss | L | 4 | 3 | 2 | 1 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| 48 | Monthly average daily solar radiation on a horizontal surface | H | 2.88 | 3.35 | 3.74 | 4.08 | 4.39 | 4.67 | 4.92 | 5.15 | 5.35 | 5.51 | 5.63 |
| 49 | Standard deviation | σ | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 | 12.01 |

Monthly-average values

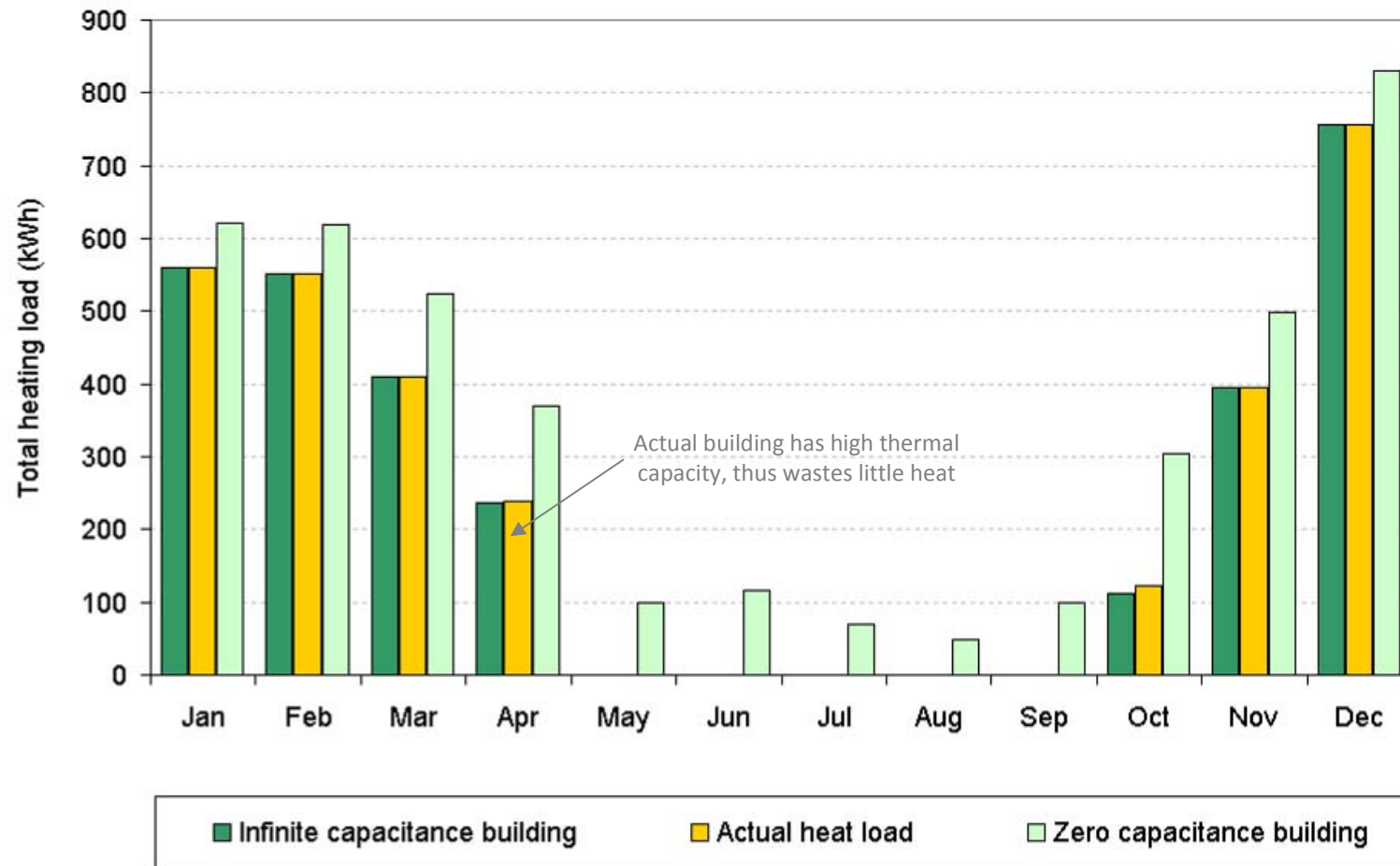
Trombe wall calculations

| | | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|---|------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 50 | Collector solar radiation data | | | | | | | | | | | | |
| 51 | Solar radiation angle (relative position of sun at solar noon) | θ | -28.52 | -24.2 | -20.1 | -16.29 | -12.63 | -9.15 | -5.84 | -2.62 | 0.5 | 3.68 | 6.81 |
| 52 | Equation of time | E | 3.78 | -16.24 | -3.55 | 8.24 | 13.91 | 8.81 | -6.81 | -14.54 | -16.45 | -10.33 | 7.64 |
| 53 | Solar time | time | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 | 19:58:08 |
| 54 | Number of daylight hours | H | 15.88 | 16.82 | 17.48 | 17.81 | 17.81 | 17.48 | 16.82 | 15.88 | 14.82 | 13.88 | 12.88 |
| 55 | Hour angle (degrees) at sunset of the sun, 15° above horizon (if appropriate) | ω _s | 2.58 | 3.75 | 4.58 | 5.05 | 5.25 | 5.05 | 4.58 | 3.75 | 2.58 | 1.58 | 0.58 |
| 56 | Transmittance factor (reference 4.16) | τ ₀ | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| 57 | Standard deviation (reference 4.16) | σ | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 | 15.51 |
| 58 | Monthly average daily solar radiation on a horizontal surface | H _h | 18.83 | 21.27 | 23.33 | 24.98 | 26.15 | 26.88 | 27.15 | 27.08 | 26.68 | 25.88 | 24.83 |
| 59 | Ratio of the diffuse solar radiation to total solar radiation on a horizontal surface | r _d | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 |
| 60 | Ratio of the diffuse solar radiation to total solar radiation on a tilted surface | r _{d,t} | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 |
| 61 | Ratio of the diffuse solar radiation to total solar radiation on a horizontal surface | r _{d,h} | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 |
| 62 | Ratio of the diffuse solar radiation to total solar radiation on a tilted surface | r _{d,t} | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 | 0.303 |
| 63 | Ratio of the beam radiation to total solar radiation on a horizontal surface | r _b | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| 64 | Ratio of the beam radiation to total solar radiation on a tilted surface | r _{b,t} | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| 65 | Ratio of radiation on a tilted surface to that on a horizontal surface | R _t | 0.76 | 0.75 | 0.85 | 0.87 | 0.88 | 0.86 | 0.85 | 0.83 | 0.83 | 0.83 | 0.85 |
| 66 | Ratio of average H/H _h | H _{h,t} | 0.75 | 0.67 | 0.68 | 0.55 | 0.55 | 0.54 | 0.55 | 0.55 | 0.57 | 0.64 | 0.74 |
| 67 | Ratio of the average daily beam radiation on the tilted surface to that on a horizontal surface | R _t | 0.75 | 0.67 | 0.68 | 0.55 | 0.55 | 0.54 | 0.55 | 0.55 | 0.57 | 0.64 | 0.74 |
| 68 | Ratio of the monthly average daily beam radiation on the tilted surface to that on a horizontal surface | R _t | 0.75 | 0.67 | 0.68 | 0.55 | 0.55 | 0.54 | 0.55 | 0.55 | 0.57 | 0.64 | 0.74 |
| 69 | Ratio of the monthly average daily beam radiation on the tilted surface to that on a horizontal surface | R _t | 0.75 | 0.67 | 0.68 | 0.55 | 0.55 | 0.54 | 0.55 | 0.55 | 0.57 | 0.64 | 0.74 |
| 70 | Monthly average daily beam radiation on a horizontal surface | H _h | 14.83 | 16.52 | 18.81 | 20.03 | 20.91 | 21.63 | 22.05 | 22.15 | 21.91 | 21.48 | 20.81 |
| 71 | Monthly average daily beam radiation on a tilted surface | H _t | 11.21 | 12.07 | 13.07 | 13.52 | 14.01 | 14.15 | 14.01 | 13.52 | 12.81 | 12.15 | 11.21 |
| 72 | Monthly average daily beam radiation on a horizontal surface | H _h | 14.83 | 16.52 | 18.81 | 20.03 | 20.91 | 21.63 | 22.05 | 22.15 | 21.91 | 21.48 | 20.81 |
| 73 | Monthly average daily beam radiation on a tilted surface | H _t | 11.21 | 12.07 | 13.07 | 13.52 | 14.01 | 14.15 | 14.01 | 13.52 | 12.81 | 12.15 | 11.21 |
| 74 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 75 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 76 | Transmittance factor (reference 4.16) | τ ₀ | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| 77 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 78 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 79 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 80 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 81 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 82 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 83 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 84 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 85 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 86 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 87 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 88 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 89 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 90 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 91 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 92 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 93 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 94 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 95 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 96 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 97 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 98 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 99 | Observed solar radiation | S | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08 | 31.58 | 31.68 | 31.38 | 30.74 |
| 100 | Monthly average solar radiation | S _h | 19.04 | 21.88 | 24.58 | 26.88 | 28.74 | 30.15 | 31.08</ | | | | |

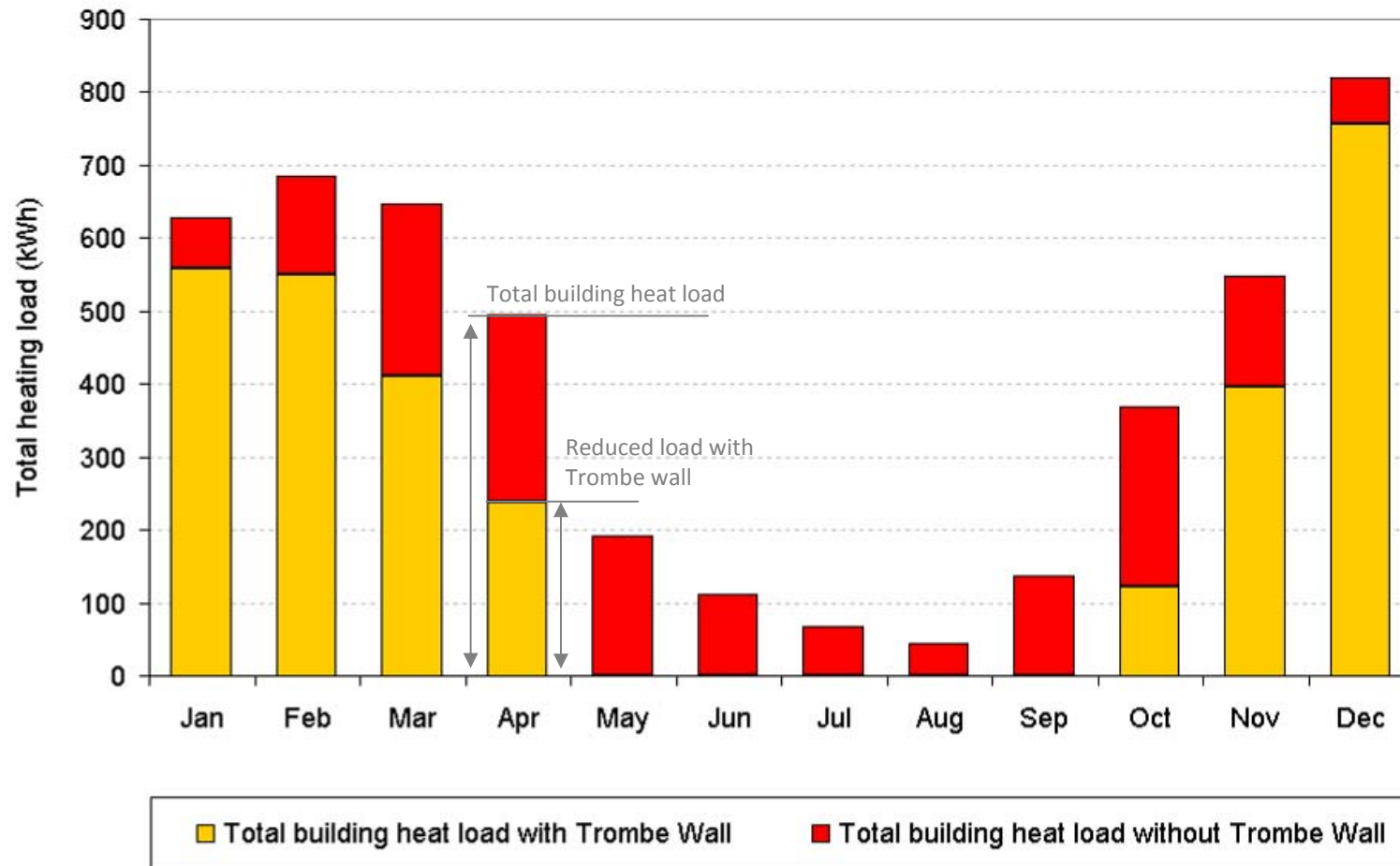
Predicted Monthly Heating Load in "Infinite" and "Zero" thermal capacitance building



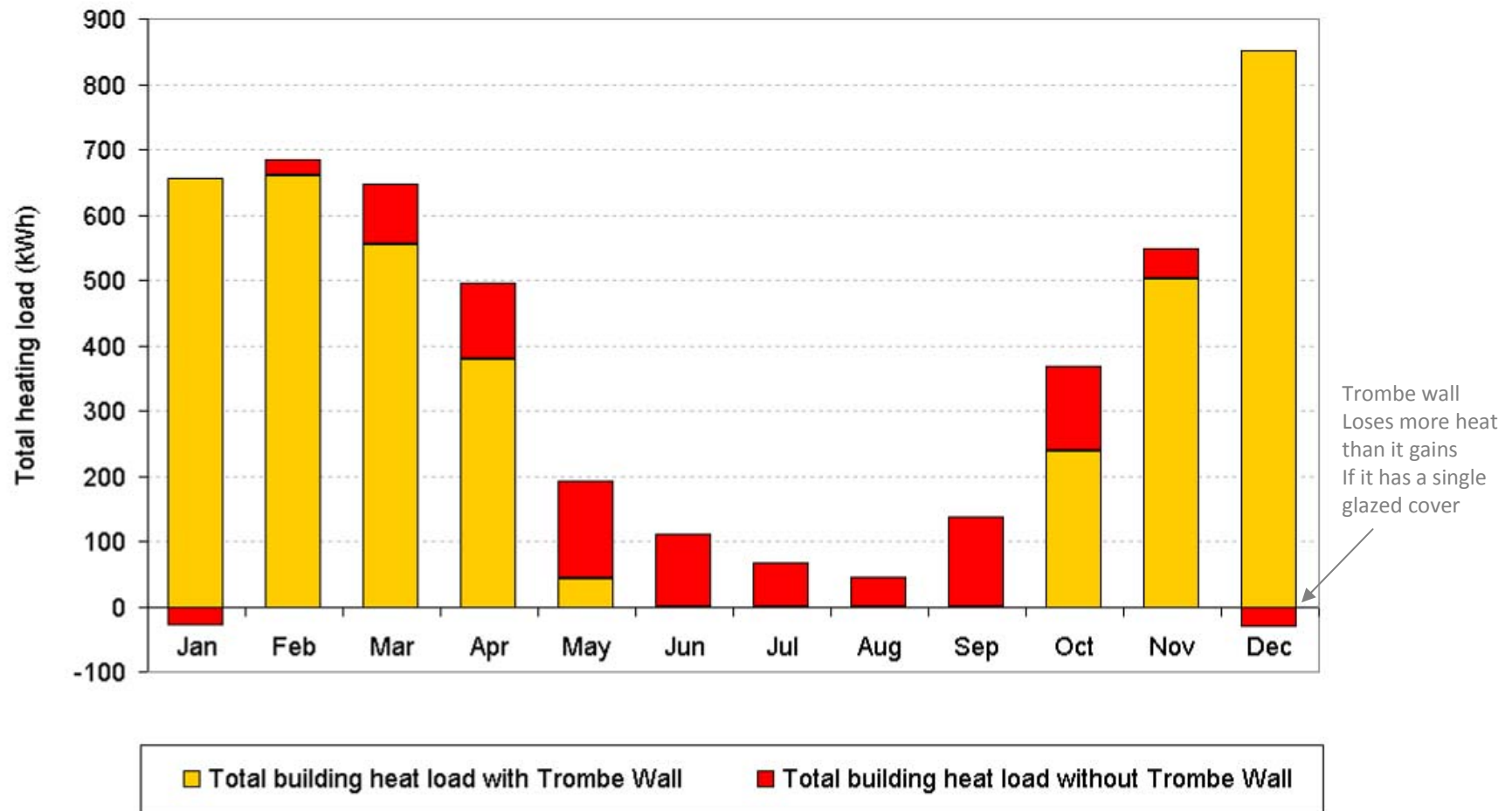
Predicted Monthly Heating Load based upon "Actual" thermal capacitance of building



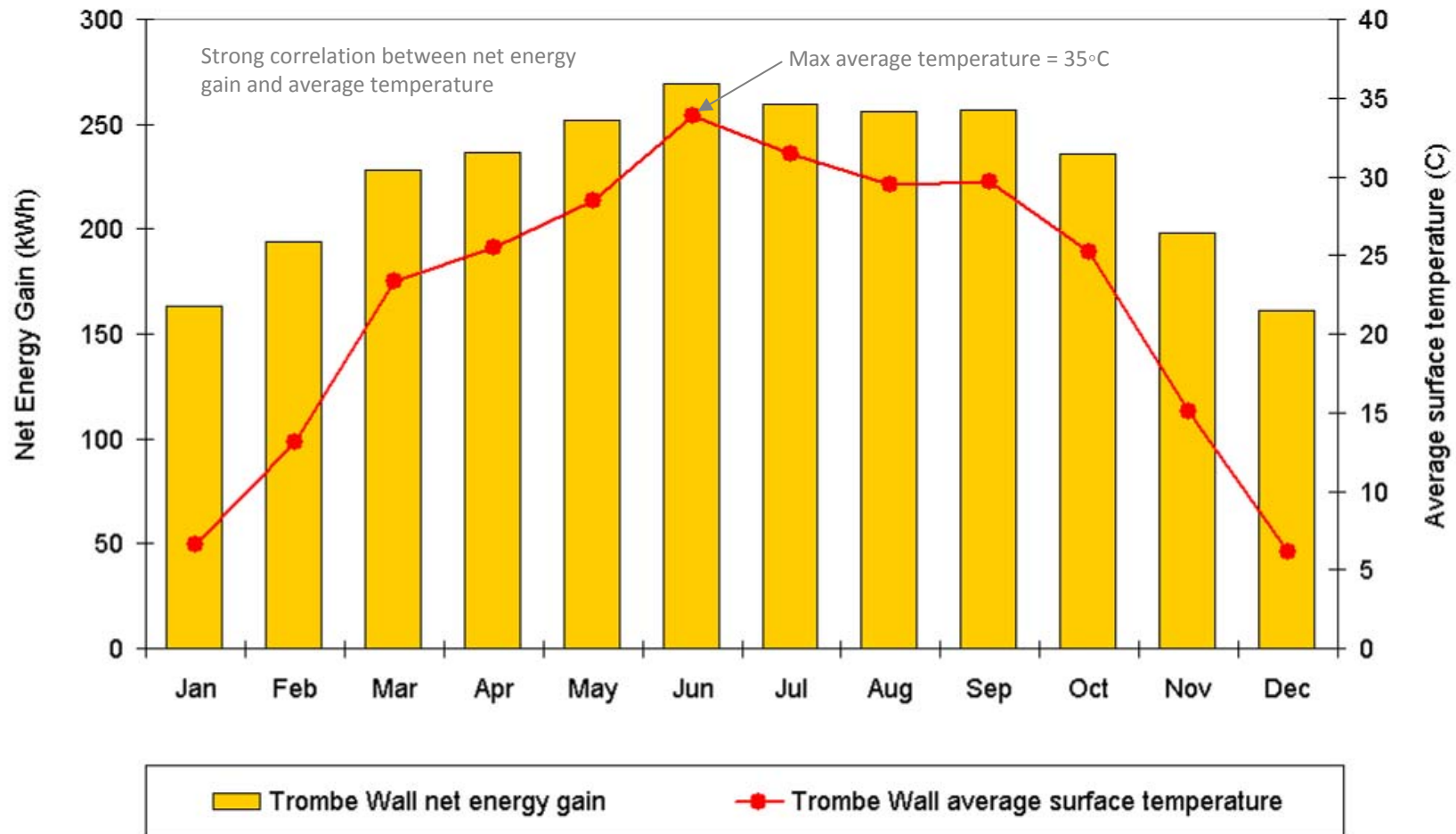
Predicted Monthly Heating Load with/without the Trombe Wall



Comparison against single glazed system

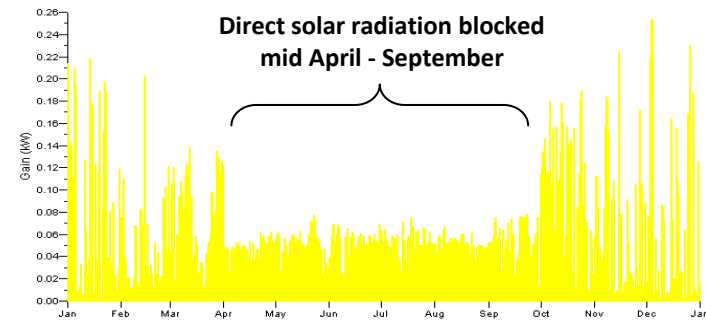
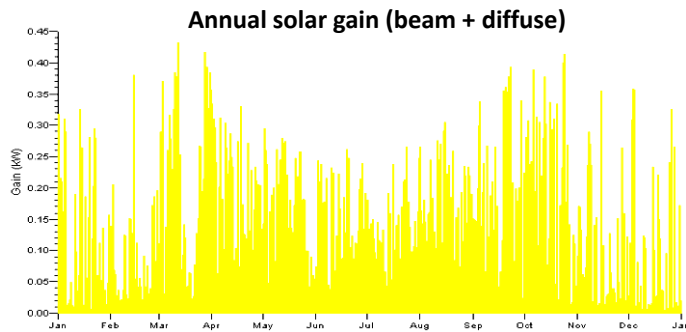
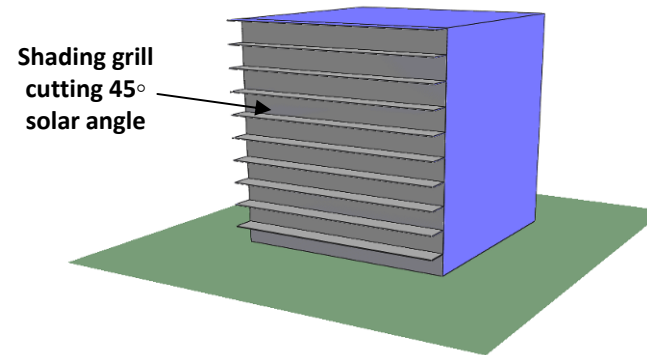
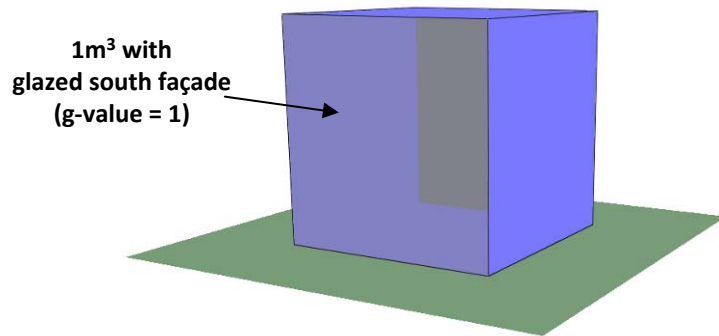


Aerogel Trombe Wall Net Energy Gain & Average Surface Temperature



Summertime overheating mitigation

- Calculator assumes wall is un-shaded, but basic modelling can demonstrate benefit of shading grill:

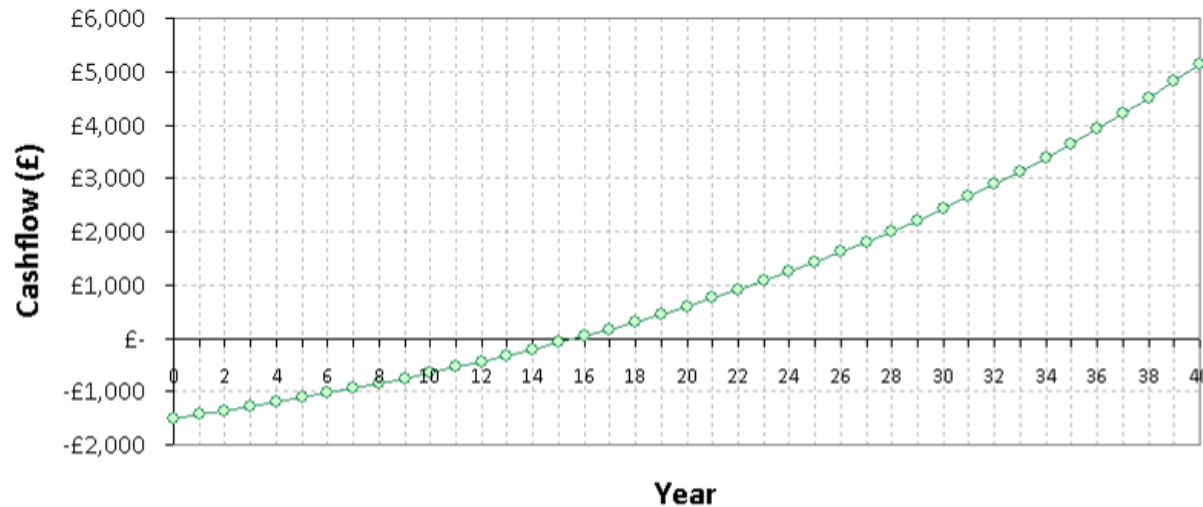




Key results:

| | | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Annual total |
|---------------------------------------|-----|------|------|------|------|------|------|------|------|------|------|------|------|---------------|
| Energy requirement (no trombe wall) | kWh | 627 | 685 | 648 | 495 | 192 | 111 | 67 | 44 | 137 | 368 | 548 | 819 | 4741 kWh/year |
| Energy requirement (with trombe wall) | kWh | 559 | 551 | 411 | 238 | 0 | 0 | 0 | 0 | 0 | 122 | 395 | 756 | 3033 kWh/year |
| Solar fraction | - | 0.14 | 0.22 | 0.39 | 0.54 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.68 | 0.30 | 0.11 | 61 % |
| Energy savings (84% efficient boiler) | kWh | 81 | 159 | 282 | 306 | 229 | 132 | 80 | 52 | 163 | 293 | 182 | 75 | 2034 kWh/year |
| Fuel bill savings (0.04p/kWh gas) | £ | 3.2 | 6.4 | 11.3 | 12.2 | 9.1 | 5.3 | 3.2 | 2.1 | 6.5 | 11.7 | 7.3 | 3.0 | 81 £/year |

Preliminary payback graph:



Assumptions

Capital cost £ 1,500
 Fuel price increase rate 6% per year
 Interest rate 2% per year

Net present value

Year 5 -£ 1,116
 Year 10 -£ 650
 Year 15 -£ 86
 Year 20 £ 598
 Year 25 £ 1,427
 Year 30 £ 2,433
 Year 35 £ 3,651
 Year 40 £ 5,127

CASE STUDY 2: Aerogel Solar Collector

- Concept currently being constructed as part of the '*Retrofit for the Future*' competition
- Property is a 3 storey 1960's end-terrace in Thamesmead, South East London
- Refurbishment strategy must achieve deep CO₂ reductions in order of 80%



Refurbishment strategy

- Aspiring towards Passivhaus certification
- Externally insulating building
- Triple glazing throughout
- Air-tight tapes on all junctions
- Mechanical ventilation with heat recovery
- DHW from boiler + solar thermal panels
- Electricity from roof mounted PVs

Gallions
Housing Association

axis

FraserBrownMacKennaArchitects

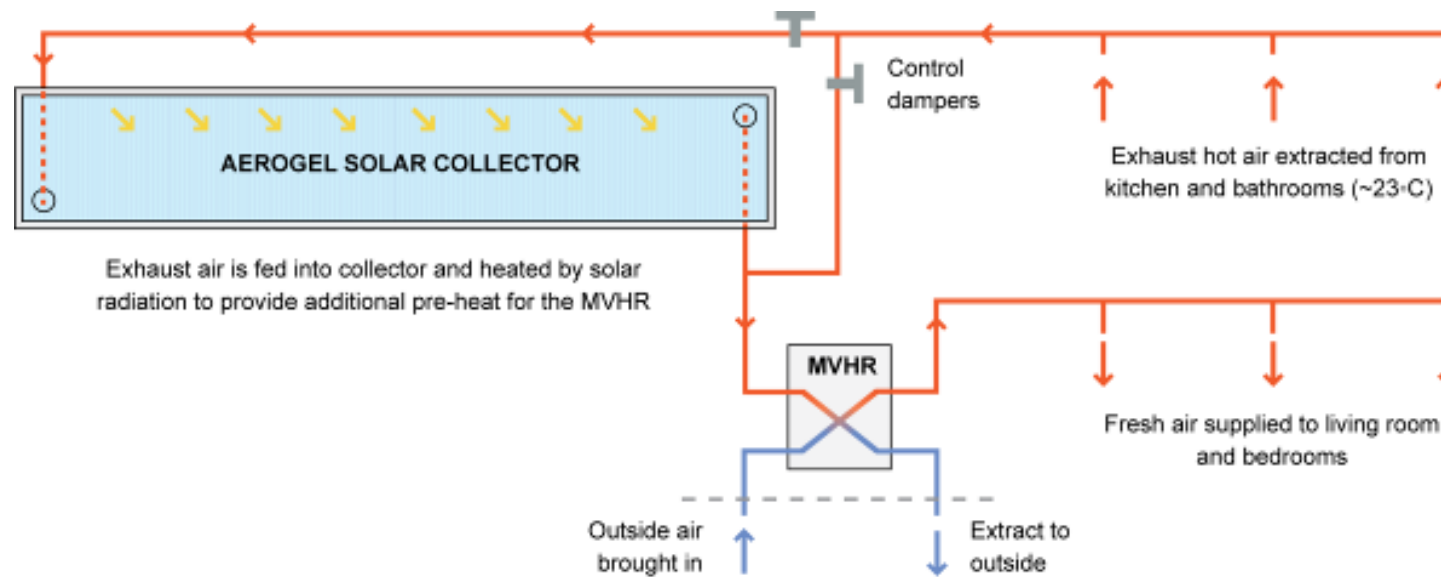


MARTIN ASSOCIATES
CHARTERED SURVEYORS



Aerogel solar collector

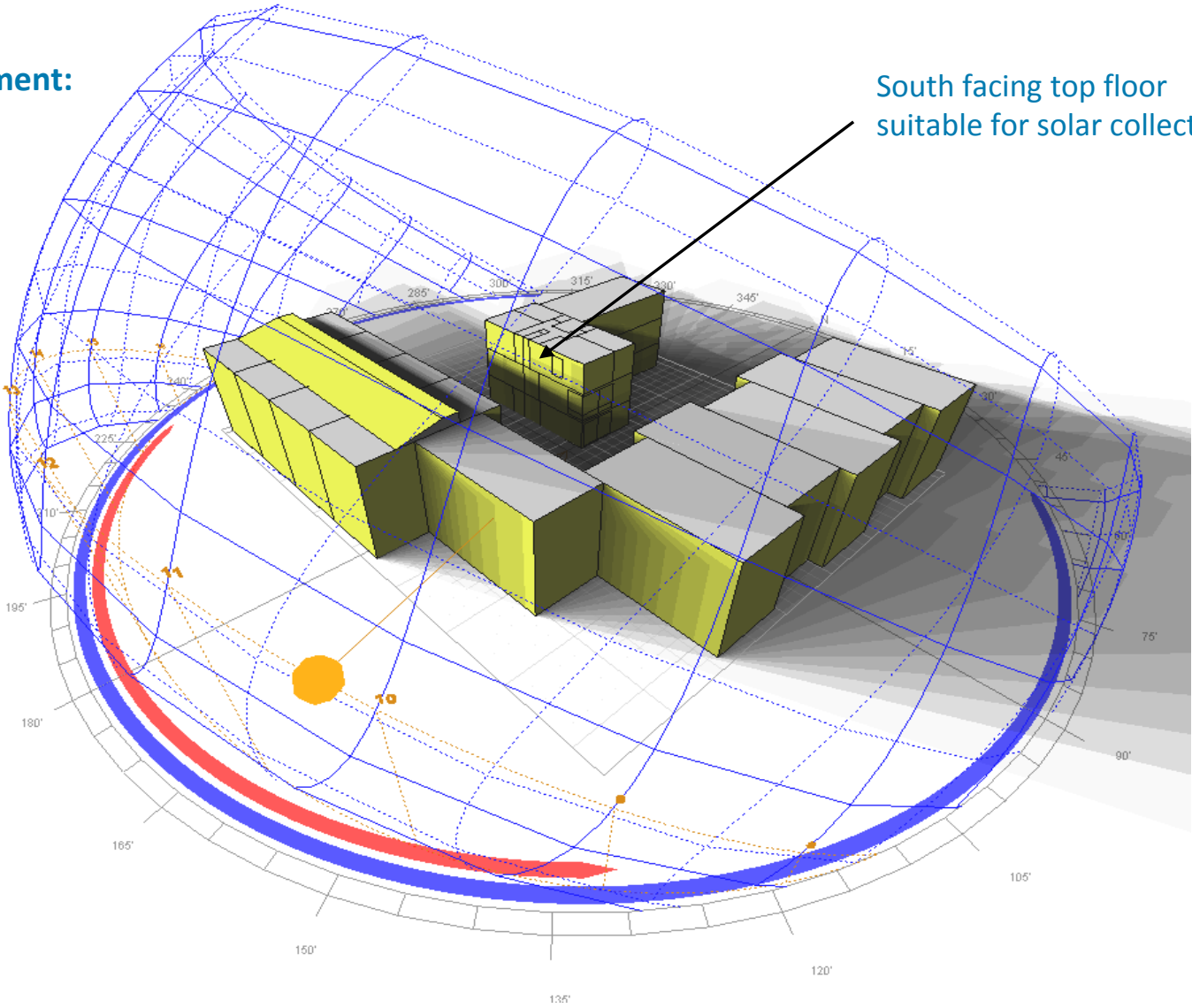
- Active solar-air system anticipated to increase the efficiency of the MVHR
- Normally an MVHR uses extracted heat from the kitchen/bathrooms to indirectly pre-heat incoming air
- Aerogel solar collector will be used to elevate this extracted air to higher temperatures





System placement:

South facing top floor
suitable for solar collector



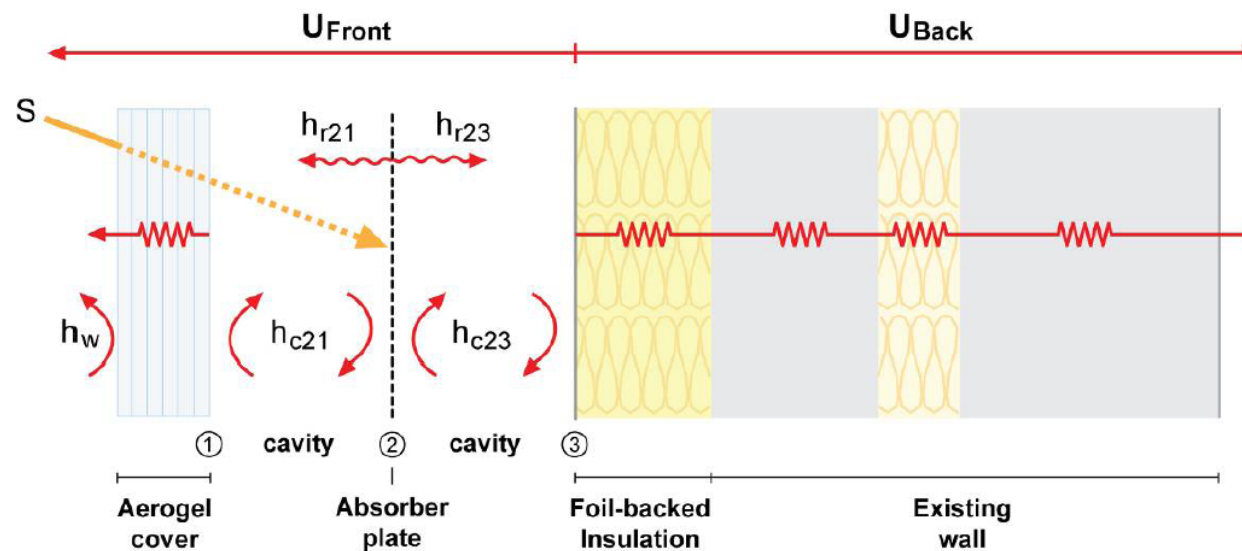
**Modelling
Validation:**



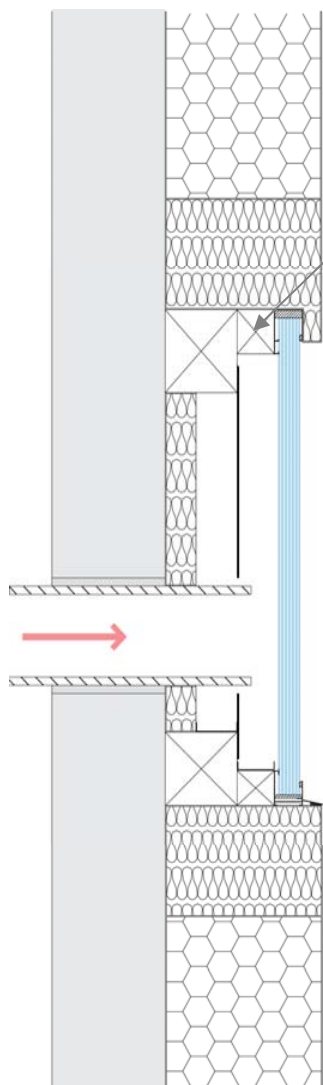
Calculation methodology:

Duffie and Beckman (2006) - Chapter 6: Flat plate solar air heater

- Parametric Excel tool combining design constants from steady state modelling with dynamic annual-hourly climate data generated using IES Virtual Environment software
- Model calculates outlet temperatures and energy generation before/after the ductwork leading to MVHR



Parametric calculator



Characterise resistance network (construction layers)

| | | Construction layers | | | | | | | | | |
|---|-----------------------|---------------------|-----------------|-----------------|----------------|---------------------|---------------------|----------------|---------------------|---------------|------|
| | | Nanogel panel | Air gap (Front) | Aluminium sheet | Air gap (Back) | Rockwool insulation | Concrete inner-leaf | EPS insulation | Concrete outer-leaf | Inner surface | |
| 1 | Thickness x | m | 0.040 | 0.080 | 0.001 | 0.080 | 0.080 | 0.080 | 0.035 | 0.105 | - |
| 2 | Conductivity k | $W/m.K$ | 0.022 | - | 250 | - | 0.035 | 1.701 | 0.040 | 1.701 | - |
| 3 | Resistance R | $m^2.K/W$ | 1.85 | - | 0 | - | 1.71 | 0.05 | 0.68 | 0.06 | 0.13 |
| 4 | Transmittance U | $W/m^2.K$ | 0.54 | - | 250000 | - | 0.58 | 21.25 | 1.14 | 16.20 | 7.69 |
| 5 | Emissivity ϵ | - | 0.85 | - | 0.68 | - | 0.10 | - | - | - | - |

Characterise weather (snapshot)

| Characterise Weather (snapshot) | | | |
|---------------------------------|-------------------------------|-------------|-----|
| Input | Output | | |
| 1 | Ambient temperature T_a | $^{\circ}C$ | 5 |
| 2 | Incident radiation θ_p | W/m^2 | 500 |
| 3 | Wind velocity v | m/s | 4 |

Characterise Collector

| Characterise Flat Plate Collector | | | |
|-----------------------------------|------------------------------------|-------------|-------|
| Input | Output | | |
| 4 | Width W | m | 6 |
| 5 | Height H | m | 0.9 |
| 6 | Tilt β | $^{\circ}$ | 90 |
| 7 | Cover transmittance τ_c | - | 0.45 |
| 8 | Plate absorptance α_p | - | 0.72 |
| 9 | Mean absorber temperature T_{pm} | $^{\circ}C$ | 46.31 |
| 10 | Mean fluid temperature T_{fm} | $^{\circ}C$ | 44.80 |

Characterise Air properties

| Characterise Heat Transfer Fluid | | | |
|----------------------------------|-----------------------------|-------------|----------|
| Input | Output | | |
| 11 | Mass flow rate \dot{m} | kg/s | 0.053 |
| 12 | Inlet air temperature T_i | $^{\circ}C$ | 25 |
| 13 | Density ρ | kg/m^3 | 1.127 |
| 14 | Specific heat C_p | $J/kg.K$ | 1007 |
| 15 | Thermal conductivity k | $W/m.K$ | 0.0272 |
| 16 | Dynamic viscosity μ | m^2/s | 1.90E-05 |
| 17 | Prandtl number Pr | - | 0.7 |

Characterise House

| Characterise House | | | |
|--------------------|-------------------------------|-------------|-----|
| Input | Output | | |
| 18 | Total volume V | m^3 | 400 |
| 19 | Internal temperature T_{in} | $^{\circ}C$ | 21 |

Characterise Ductwork

| Characterise duct leaving collector | | | |
|-------------------------------------|---------------------------------|---------|-------|
| Input | Output | | |
| 20 | Duct diameter D | m | 0.15 |
| 21 | Duct length L | m | 10 |
| 22 | Insulation thickness Δx | m | 0.03 |
| 23 | Insulation conductivity k | $W/m.K$ | 0.035 |

Characterise MVHR

| Characterise MVHR | | | |
|-------------------|--|-----|-----|
| Input | Output | | |
| 24 | Heat exchange efficiency η_{MVHR} | m | 85% |

Performance calculations

| Calculations | | | |
|--------------|-----------------------------------|-------------|------------|
| Input | Output | | |
| 1 | Stefan boltzman constant σ | - | 5.67E-08 |
| 2 | Hydraulic diameter D_h | m | 0.16 |
| 3 | Reynolds number Re | - | 3823 |
| 4 | Flow regime? | - | Transition |
| 5 | Nusselt number Nu | - | - |
| 6 | Laminar | - | 10.25 |
| 7 | Turbulent | - | 11.60 |
| 8 | Selection: | - | 11.60 |
| 9 | Wind co-efficient h_{wv} | $W/m^2.K$ | 8.89 |
| 10 | Convection co-efficient h_{c12} | $W/m^2.K$ | 1.97 |
| 11 | Convection co-efficient h_{c23} | $W/m^2.K$ | 1.97 |
| 12 | Radiation co-efficient h_{r12} | $W/m^2.K$ | 5.55 |
| 13 | Radiation co-efficient h_{r23} | $W/m^2.K$ | 0.72 |
| 14 | Back losses U_b | $W/m^2.K$ | 0.35 |
| 15 | Front losses U_f | $W/m^2.K$ | 0.46 |
| 16 | Overall losses U_L | $W/m^2.K$ | 0.77 |
| 17 | Collector efficiency factor F' | - | 0.94 |
| 18 | Capacitance rate | - | 8.51 |
| 19 | Collector flow factor F'' | - | 0.94 |
| 20 | Heat removal factor F_R | - | 0.88 |
| 21 | Area of outlet ducting A_o | m^2 | 4.71 |
| 22 | Loss co-efficient of ducts U_d | $W/m^2.K$ | 1.17 |
| 23 | Temperature drop from ducts T_d | $^{\circ}C$ | 4.01 |

Air flow properties

Heat loss co-efficients

Efficiency factors

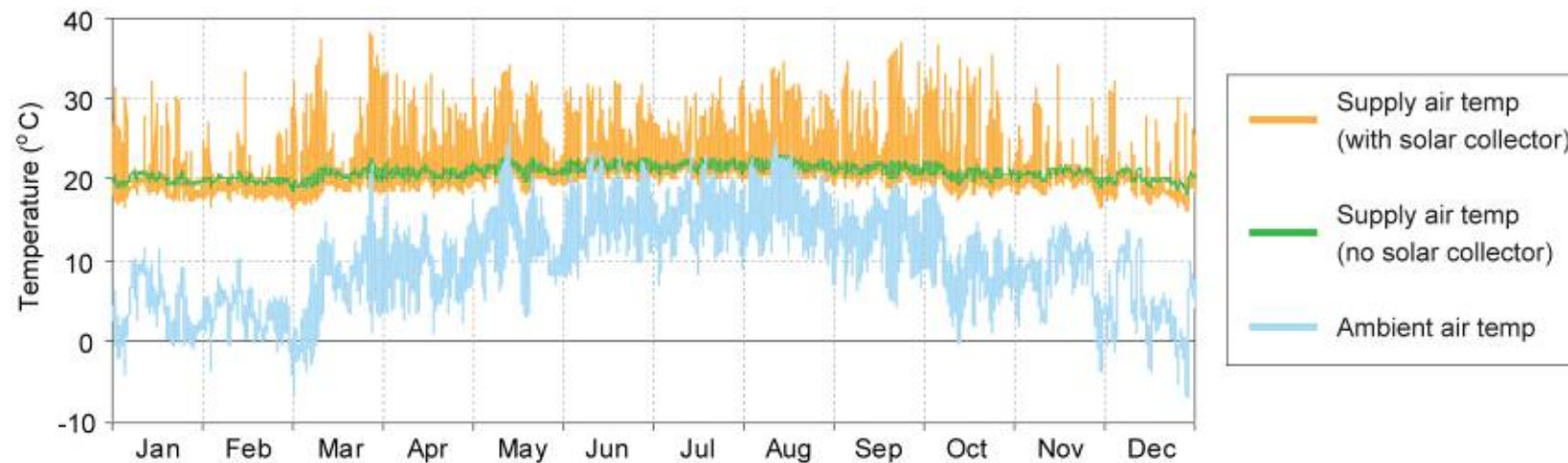
Ductwork losses

| Key Results | | | |
|---|--|-------------|--------|
| Input | Output | | |
| 21 | Useful energy Q_u | W | 723.58 |
| 22 | Outlet temperature T_o | $^{\circ}C$ | 44.98 |
| 23 | Mean plate temperature T_{pm} | $^{\circ}C$ | 45.31 |
| 24 | Mean fluid temperature T_{fm} | $^{\circ}C$ | 44.80 |
| 25 | Instantaneous efficiency η_i | $\%$ | 0.27 |
| Effect of ductwork leaving collector | | | |
| 26 | Useful energy Q_u | W | 591.57 |
| 27 | Outlet temperature T_o | $^{\circ}C$ | 40.97 |
| Supply temperature to house | | | |
| 28 | Basecase (no solar collector) T_s | $^{\circ}C$ | 20.30 |
| 29 | Supply temp with solar collector T_s | $^{\circ}C$ | 35.59 |

Summary table of key results

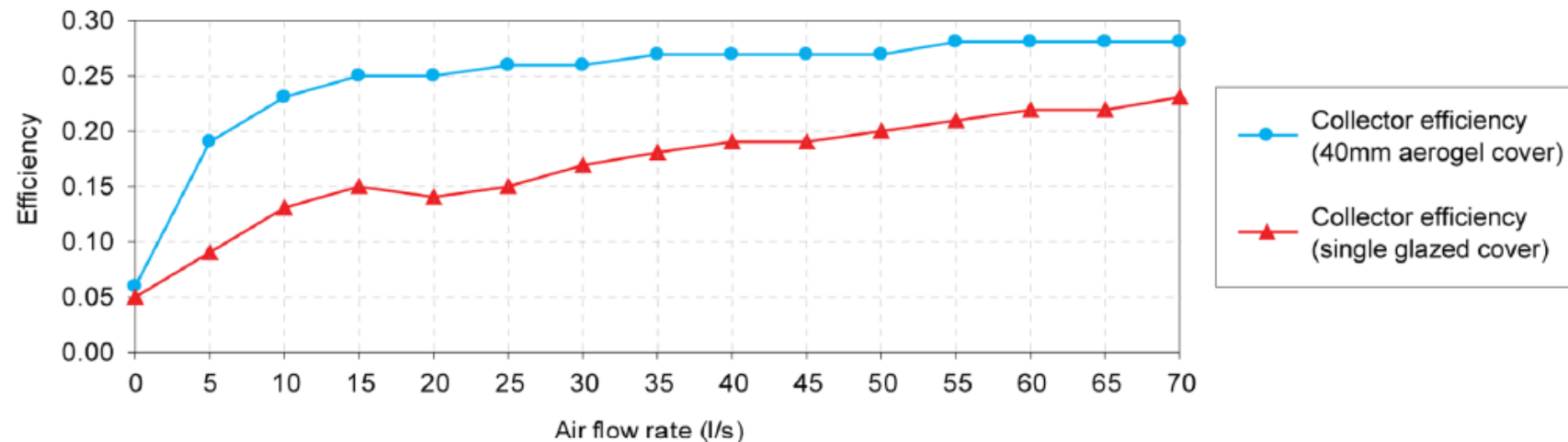
Predicted supply air temperatures:

- Predicted supply-air temperatures up to 30°C on cold-mild sunny days
- Peak temperatures up to 40°C in March & September indicating bypass controls required



- Note that supply air temperatures without solar collector are predicted between 18-21 °C
- However, this may not be accurate as model assumes constant flow rate & exhaust air temp of 23°C

Efficiency compared to single glazed system:



Notes on efficiency:

- System located on vertical wall – not at 30° pitch
- System inlet temperature – higher efficiency occurs if system heats ambient air directly
- Absorber sheet is perforated – efficiency calculation assumes absorption area is reduced

Next steps:

- Construction
- Monitoring
- Validation



Installation of solar
collector frame:



**Installation of
pre-fabricated
ductwork:**



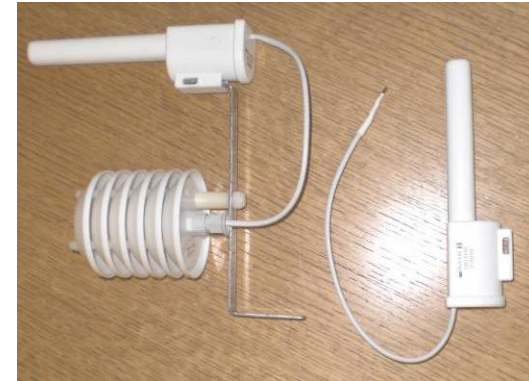
**Aerogel panels,
absorber sheet
MVHR + flow
control dampers:**



Monitoring & Validation:

- Whole house
 - Gas, electricity + water consumption
 - Internal + external temperatures and humidity
 - Performance of renewable technologies

- Aerogel solar collector:



S





Thank you for listening

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Modelling Reference:

Duffie and Beckman (2006), Solar Engineering of Thermal Processes

Third Edition, John Wiley & Sons Inc, New York, USA